

### **Computational Modeling and Optimization of Proton Exchange Membrane Fuel Cells using deal.ii**

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### Introduction







### Introduction

- Fuel cells are governed by several coupled physical phenomena
- Fuel cell performance depends on a large number of coupled design parameters
- Numerical optimization allows changing of all design parameters simultaneously to obtain an optimal design



### **Previous work**

- Song et al., 2004
  - One-dimensional catalyst layer model
  - Gradient-based method with numerical sensitivities
- Gurujicic et al., 2004
  - Two- and three-dimensional fuel cell with a zerothickness catalyst layer model
  - Gradient-based method with numerical sensitivities
- Mawardi et al., 2005
  - One-dimensional fuel cell model
  - Nelder-Mead simplex method combined with simulated annealing optimization



### **Previous work**

- Limited to a low accuracy fuel cell model due to the computational expense of solving high-fidelity models
- This limitation can be reduced by using
  - parallel machine architecture
  - gradient-based methods
  - efficient method to compute the gradients





### Objectives

- Development of an optimization framework for high-fidelity fuel cell models by using
  - accurate two-dimensional fuel cell models solved using deal.ii
  - gradient-based optimization algorithms coupled with analytical sensitivities obtained using deal.ii





## Methodology

- In order to develop a numerical fuel cell optimization framework it is necessary to develop
  - Accurate fuel cell model
  - A program using deal.ii to solve the fuel cell model
  - Appropriate objective function and constraints
  - Objective function and constraints analytical sensitivities
  - Optimization algorithm





Fuel cell model

- Develop the set of partial differential equations (PDE) that governs the fuel cell R(u, p) = 0
- Solve the governing equations using the deal.ii finite element library
- Adaptive mesh refinement
- Parallel solution of the equations





# **Design problem**

- Perform a parametric study and select
  - $\checkmark$  objective function
    - maximize current density
    - maximize power
  - ✓ constraints/requirements
    - limit maximum cell temperature
    - limit maximum amount of platinum
  - ✓ design variables
    - geometric variables
    - composition variables
    - operating variables





Analytical sensitivities

• Gradients of objective function and constraints, *f*, are given by

df(u,p)	_	$\partial f(u,p)$	$\partial u$		$\partial f(u,p)$
dp	_	$\partial u$	$\overline{\partial p}$	Т	$\partial p$

• Differentiate the fuel cell governing equations with respect to the design parameters

$$\frac{\partial R(u,p)}{\partial u} \ \frac{\partial u}{\partial p} = -\frac{\partial R(u,p)}{\partial p}$$



### **Optimization framework**





### **Catalyst layer optimization**

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### **Problem formulation**

- One dimensional catalyst layer composition optimization
- Optimization problem is to

 $\begin{array}{ll} \text{minimize} & overpotential(\eta(i=i_0)) \\ \text{w.r.t.} & \epsilon_N, m_{Pt} \\ \text{subject to:} & 0 \leq \epsilon_V \leq 1 \\ & 0 \leq \epsilon_S \leq 1 \\ & 0 \leq \epsilon_N \leq 1 \end{array}$ 



### 1D catalyst layer model

$$nFD_{O_{2}}^{eff} \frac{d^{2}c_{O_{2}}}{dx^{2}} = \frac{di}{dx} = f(c_{O_{2}}, \eta)$$
$$\left(\frac{-1}{\frac{1}{\sigma_{N}^{eff}} + \frac{1}{\sigma_{S}^{eff}}}\right) \frac{d^{2}\eta}{dx^{2}} = \frac{di}{dx} = f(c_{O_{2}}, \eta)$$

where

$$f(c_{O_2},\eta) = \frac{di}{dx} = i_0^{ref} \left(\frac{c_{O_2}}{c_{O_2}^{ref}}\right)^{\gamma} \exp\left(\frac{\alpha F}{RT}\eta\right)$$



### **Boundary conditions**







### Finite element solution

• Use Newton method to solve the system. The linearized equations are

$$\frac{dR(u,\lambda)}{du}\delta u = -R(u,\lambda)$$

- The linerized problem is solved using
  - the Galerkin method
  - first order elements
  - Global refinement





### **Optimization process**

- The gradient of the overpotential and constraints is obtained by analytical differentiation of the governing equations
- The Modified Method of Feasible Directions is used to solve the optimization problem





### **Problem initial parameters**

• Current density:

 $-i_0 = 0.5 \text{A/cm}^2$ 

- Initial Design:
  - Objective:
    - $\eta = -0.675514 V$
  - Design variables:
    - $m_{Pt} = 3.332 \times 10^{-4} \text{ g cm}^{-2}$
    - $\epsilon_{\rm N} = 0.3$





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### **Optimization results**

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 $\checkmark \eta = -0.657852 V$ 

 $\checkmark$  m<sub>Pt</sub> = 1.989x10<sup>-4</sup> g cm<sup>-2</sup>,  $\varepsilon_{\rm N}$  = 0.597806





### **Post-optimal analysis**

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• Solution sensitivity to changes in design variables







### **Problem formulation**

- Two dimensional electrode composition optimization
- Optimization problem is to

 $\begin{array}{ll} \text{maximize} & i(dV=V_0) \\ \text{w.r.t.} & \epsilon_V^{GDL}, \epsilon_N^{CAT}, m_{Pt}, \% Pt \\ \text{subject to:} & 0 \leq \epsilon_V \leq 1 \\ & 0 \leq \epsilon_S \leq 1 \\ & 0 \leq \epsilon_N \leq 1 \end{array}$ 



# Two-dimensional cathode electrode problem

 $\nabla \cdot (cD_{O_2}^{eff} \nabla x_{O_2}) = \frac{1}{4F} \nabla \cdot \vec{i}$   $\nabla \cdot (\sigma_m^{eff} \nabla \phi_m) = \nabla \cdot \vec{i}$   $\nabla \cdot (\sigma_S^{eff} \nabla \phi_S) = -\nabla \cdot \vec{i}$ 

where

$$\nabla \cdot \vec{i} = i_0^{ref} \left( \frac{cx_{O_2}}{c_{O_2}^{ref}} \right)^{\gamma} \exp\left( \frac{\alpha F}{RT} (\phi_m - \phi_S) \right)$$



### **Boundary conditions**

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### **Finite element solution**

• Use Newton method to solve the system of equations. The linearized equations are

$$\frac{dR(u,\lambda)}{du}\delta u = -R(u,\lambda)$$

- The linerized problem is solved using
  - the Galerkin method
  - first order elements
  - adaptive grid refinement





### **Current density**

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• The current density is obtained in the post-analysis using either

$$i = \frac{1}{H} \int_0^H \int_0^L RRdxdy =$$
  
=  $\frac{1}{H} \int_0^H \int_0^L i_0^{ref} \left(\frac{cx_{O_2}}{c_{O_2}^{ref}}\right)^\gamma \exp\left(\frac{\alpha F}{RT}(\phi_m - \phi_S)\right) dxdy$ 

or





### Adaptive grid refinement

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- Kelly error estimator for  $c_{o_2}$  and  $\phi_S$ 





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### **Catalyst layer solution**



Contour lines at the catalyst layer for i=0.4A/cm<sup>2</sup> and  $\sigma_s = 0.53$  S/cm of (a) oxygen molar fraction [-], (b) potential in the solid phase [V], (c) potential in the electrolyte [V] and (d) reaction rate [A/cm<sup>3</sup>]



### **Optimization solution**

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- Initial Design:
  - Objective:
    - $i = 0.491367 \text{ A/cm}^2 \text{ for } dV = 0.25 \text{ V}$
  - Design variables:
    - GDL :  $\varepsilon_V = 0.5$
    - CL:  $m_{Pt} = 3.332 \times 10^{-4} \text{ g cm}^{-2}$
    - CL:  $\epsilon_{\rm N} = 0.3$
    - CL: %Pt = 0.2
  - Grid with a maximum of 500 dof => preliminary results!





### **Optimization solution**

- Final Design:
  - Objective:
    - $i = 1.01408 \text{ A/cm}^2 \text{ for } dV = 0.25 \text{ V}$
  - Design variables:
    - GDL :  $\varepsilon_V = 0.620494 \Longrightarrow \sim 25\%$  increase
    - CL:  $m_{Pt} = 10.3464 \times 10^{-4} \text{ g cm}^{-2} => \sim 200\%$  increase
    - CL:  $\epsilon_N = 0.424708 \implies \sim 30\%$  increase
    - CL: %Pt = 0.463985 => ~60% increase

The current density has doubled!!!



### Summary

- Deal.ii was successfully used
  - to solve one and two-dimensional fuel cell models involving highly nonlinear source terms
  - to obtain the analytical sensitivities of the unknowns of the analysis problem and the objective function of the optimization problem
  - to perform fuel cell optimization in conjunction with a commercial optimization software





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# **Thank You**

